# 1.1 GHz PLL Frequency Synthesizers 

## Include On-Board 64/65 Prescalers

The MC145190 and MC145191 are single-package synthesizers with serial interfaces capable of direct usage up to 1.1 GHz . A special architecture makes these PLLs very easy to program because a byte-oriented format is utilized. Due to the patented BitGrabber ${ }^{T M}$ registers, no address/steering bits are required for random access of the three registers. Thus, tuning can be accomplished via a 3-byte serial transfer to the 24-bit A register. The interface is both SPI and MICROWIRE ${ }^{\text {TM }}$ compatible.

Each device features a single-ended current source/sink phase detector output and a double-ended phase detector output. Both phase detectors have linear transfer functions (no dead zones). The maximum current of the single-ended phase detector output is determined by an external resistor tied from the Rx pin to ground. This current can be varied via the serial port.

The MC145190 features logic-level converters and high-voltage phase/ frequency detectors; the detector supply may range up to 9.5 V . The MC145191 has lower-voltage phase/frequency detectors optimized for single-supply systems of $5 \mathrm{~V} \pm 10 \%$.

Each part includes a differential RF input which may be operated in a single-ended mode. Also featured are on-board support of an external crystal and a programmable reference output. The $R, A$, and $N$ counters are fully programmable. The C register (configuration register) allows the parts to be configured to meet various applications. A patented feature allows the C register to shut off unused outputs, thereby minimizing system noise and interference.

In order to have consistent lock times and prevent erroneous data from being loaded into the counters, on-board circuitry synchronizes the update of the A register if the A or N counters are loading. Similarly, an update of the R register is synchronized if the $R$ counter is loading.

The double-buffered $R$ register allows new divide ratios to be presented to the three counters ( $R, A$, and $N$ ) simultaneously.

- Maximum Operating Frequency: $1100 \mathrm{MHz} @ \mathrm{~V}_{\text {in }}=200 \mathrm{mV}$ p-p
- Operating Supply Current: 7 mA Nominal
- Operating Supply Voltage Range (VDD and $\mathrm{V}_{\mathrm{CC}}$ Pins): 4.5 to 5.5 V
- Operating Supply Voltage Range of Phase Detectors (VPD Pin) -

MC145190: 8.0 to 9.5 V
MC145191: 4.5 to 5.5 V

- Current Source/Sink Phase Detector OUTPUT Capability: 2 mA Maximum
- Gain of Current Source/Sink Phase/Frequency Detector Controllable via Serial Port
- Operating Temperature Range: -40 to $+85^{\circ} \mathrm{C}$
- R Counter Division Range: (1 and) 5 to 8191
- Dual-Modulus Capability Provides Total Division up to 262,143
- High-Speed Serial Interface: 4 Mbps
- OUTPUT A Pin, When Configured as Data Out, Permits Cascading of Devices
- Two General-Purpose Digital Outputs - OUTPUT A: Totem-Pole (Push-Pull) OUTPUT B: Open-Drain
- Patented Power-Saving Standby Feature with Orderly Recovery for

Minimizing Lock Times, Standby Current: $30 \mu \mathrm{~A}$

- Evaluation Kit Available (Part Numbers MC145190EVK and MC145191EVK)
- See Application Note AN1253/D for Low-Pass Filter Design, and AN1277/D for Offset Reference PLLs for Fine Resolution or Fast Hopping

BitGrabber is a trademark of Motorola Inc. MICROWIRE is a trademark of National Semiconductor Corp.

## BLOCK DIAGRAM



MAXIMUM RATINGS＊（Voltages Referenced to GND，unless otherwise stated）

| Symbol | Parameter | Value | Unit |
| :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\mathrm{CC}}$ ， <br> VD | DC Supply Voltage（Pins 12 and 14） | -0.5 to＋6．0 | V |
| $\mathrm{V}_{\mathrm{PD}}$ | $\begin{array}{ll}\text { DC Supply Voltage（Pin 5）} & \text { MC145190 } \\ & \text { MC145191 }\end{array}$ | $\begin{array}{\|l} \hline \mathrm{V}_{\mathrm{DD}}-0.5 \text { to }+9.5 \\ \mathrm{~V}_{\mathrm{DD}}-0.5 \text { to }+6.0 \end{array}$ | V |
| $\mathrm{V}_{\text {in }}$ | DC Input Voltage | -0.5 to $\mathrm{V}_{\mathrm{DD}}+0.5$ | V |
| $V_{\text {out }}$ | DC Output Voltage（except OUTPUT B，PD out，申R，申V） | -0.5 to $\mathrm{V}_{\mathrm{DD}}+0.5$ | V |
| $V_{\text {out }}$ | DC Output Voltage（OUTPUT B，PD ${ }_{\text {out }}$ ，¢R，¢V） | -0.5 to $\mathrm{V}_{\mathrm{PD}}+0.5$ | V |
| $\mathrm{l}_{\text {in }}$ ，IPD | DC Input Current，per Pin（Includes $\mathrm{V}_{\text {PD }}$ ） | $\pm 10$ | mA |
| Iout | DC Output Current，per Pin | $\pm 20$ | mA |
| IDD | DC Supply Current，V ${ }_{\text {DD }}$ and GND Pins | $\pm 30$ | mA |
| PD | Power Dissipation，per Package | 300 | mW |
| $\mathrm{T}_{\text {stg }}$ | Storage Temperature | -65 to＋ 150 | ${ }^{\circ} \mathrm{C}$ |
| TL | Lead Temperature， 1 mm from Case for 10 seconds | 260 | ${ }^{\circ} \mathrm{C}$ |

＊Maximum Ratings are those values beyond which damage to the device may occur． Functional operation should be restricted to the limits in the Electrical Characteristics tables or Pin Descriptions section．

This device contains protection circuitry to guard against damage due to high static volt－ ages or electric fields．However，precautions must be taken to avoid applications of any volt－ age higher than maximum rated voltages to this high－impedance circuit．

## ELECTRICAL CHARACTERISTICS

$\left(\mathrm{V}_{\mathrm{DD}}=\mathrm{V}_{\mathrm{CC}}=4.5\right.$ to 5.5 V , Voltages Referenced to $\mathrm{GND}, \mathrm{T}_{\mathrm{A}}=-40$ to $+85^{\circ} \mathrm{C}$, unless otherwise stated;
MC145190: $\mathrm{V}_{\mathrm{PD}}=8.0$ to 9.5 V ; MC145191: $\mathrm{V}_{\mathrm{PD}}=4.5$ to 5.5 V with $\mathrm{V}_{\mathrm{DD}} \leq \mathrm{V}_{\mathrm{PD}}$.)

| Symbol | Parameter | Test Condition | Guaranteed Limit | Unit |
| :---: | :---: | :---: | :---: | :---: |
| VIL | Maximum Low-Level Input Voltage ( $\mathrm{D}_{\text {in }}, \mathrm{CLK}, \mathrm{ENB}$, REF $_{\text {in }}$ ) | Device in Reference Mode, dc Coupled | $0.3 \times \mathrm{V}_{\text {D }}$ | V |
| $\mathrm{V}_{\mathrm{IH}}$ | Minimum High-Level Input Voltage ( $\mathrm{D}_{\mathrm{in}}, \mathrm{CLK}, \mathrm{ENB}, \mathrm{REF}_{\text {in }}$ ) | Device in Reference Mode, dc Coupled | $0.7 \times \mathrm{V}_{\mathrm{DD}}$ | V |
| $\mathrm{V}_{\text {hys }}$ | Minimum Hysteresis Voltage (CLK, ENB) |  | 300 | mV |
| VOL | Maximum Low-Level Output Voltage ( REF $_{\text {out }}$, OUTPUT A) | Iout $=20 \mu \mathrm{~A}$, Device in Reference Mode | 0.1 | V |
| $\mathrm{V}_{\mathrm{OH}}$ | Minimum High-Level Output Voltage (REF ${ }_{\text {out }}$, OUTPUT A) | Iout $=-20 \mu \mathrm{~A}$, Device in Reference Mode | $\mathrm{V}_{\mathrm{DD}}-0.1$ | V |
| ${ }^{\text {IOL }}$ | Minimum Low-Level Output Current ( $\mathrm{REF}_{\text {out }}, \mathrm{LD}, \phi \mathrm{R}, \phi \mathrm{V}$ ) | $\mathrm{V}_{\text {out }}=0.4 \mathrm{~V}$ | 0.36 | mA |
| ${ }^{\mathrm{I} O H}$ | Minimum High-Level Output Current ( $\mathrm{REF}_{\text {out }}, \mathrm{LD}, \phi \mathrm{R}, \phi \mathrm{V}$ ) | $\begin{aligned} & V_{\text {out }}=V_{D D}-0.4 \mathrm{~V} \text { for } R E F_{\text {out }}, L D \\ & V_{\text {out }}=V_{\text {PD }}-0.4 \mathrm{~V} \text { for } \phi R, \phi \mathrm{~V} \end{aligned}$ | -0.36 | mA |
| ${ }^{\text {IOL}}$ | Minimum Low-Level Output Current (OUTPUT A, OUTPUT B) | $\mathrm{V}_{\text {out }}=0.4 \mathrm{~V}$ | 1.0 | mA |
| ${ }^{\mathrm{I} O H}$ | Minimum High-Level Output Current (OUTPUT A, Only) | $\mathrm{V}_{\text {out }}=\mathrm{V}_{\mathrm{DD}}-0.4 \mathrm{~V}$ | -0.6 | mA |
| lin | Maximum Input Leakage Current ( $\mathrm{D}_{\text {in }}, \mathrm{CLK}, \mathrm{ENB}, \mathrm{REF}_{\text {in }}$ ) | $\mathrm{V}_{\text {in }}=\mathrm{V}_{\text {DD }}$ or GND, Device in XTAL Mode | $\pm 1.0$ | $\mu \mathrm{A}$ |
| lin | Maximum Input Current ( $\mathrm{REF}_{\text {in }}$ ) | $\mathrm{V}_{\text {in }}=\mathrm{V}_{\text {DD }}$ or GND, Device in Reference Mode | $\pm 150$ | $\mu \mathrm{A}$ |
| IOZ | Maximum Output Leakage Current ( $\mathrm{PD}_{\text {out }}$ ) | $\mathrm{V}_{\text {out }}=\mathrm{V}_{\text {PD }}-0.5 \mathrm{~V}$ or 0.5 V, MC145190 <br> Output in High-Impedance State MC145191 | $\begin{aligned} & \pm 150 \\ & \pm 200 \end{aligned}$ | nA |
| IOZ | Maximum Output Leakage Current (OUTPUT B) | $V_{\text {out }}=V_{\text {PD }}$ or GND, Output in High-Impedance State | $\pm 10$ | $\mu \mathrm{A}$ |
| ISTBY | Maximum Standby Supply Current ( $V_{D D}+V_{P D}$ Pins) | $\mathrm{V}_{\text {in }}=\mathrm{V}_{\text {DD }}$ or GND; Outputs Open; Device in Standby Mode, Shut-Down Crystal Mode or REF out-Static-Low $^{\text {L }}$ Reference Mode; OUTPUT B Controlling $\mathrm{V}_{\mathrm{CC}}$ per Figure 22 | 30 | $\mu \mathrm{A}$ |
| ${ }^{\text {IPD }}$ | Maximum Phase Detector Quiescent Current (VPD Pin) | Bit C6 = High Which Selects Phase Detector A, <br> PD ${ }_{\text {out }}=$ Open, $\mathrm{PD}_{\text {out }}=$ Static Low or High, Bit C4 = Low Which is not Standby, $\mathrm{I}_{\mathrm{Rx}}=113 \mu \mathrm{~A}$ | 600 | $\mu \mathrm{A}$ |
|  |  | Bit C6 = Low Which Selects Phase Detector B, $\phi$ R and $\phi V=$ Open, $\phi \mathrm{R}$ and $\phi \mathrm{V}=$ Static Low or High, Bit C4 = Low Which is not Standby | 30 |  |
| ${ }^{1} \mathrm{~T}$ | Total Operating Supply Current $\left(\mathrm{V}_{\mathrm{DD}}+\mathrm{V}_{\mathrm{PD}}+\mathrm{V}_{\mathrm{CC}}\right.$ Pins $)$ | $\mathrm{f}_{\mathrm{in}}=1.1 \mathrm{GHz} ; \mathrm{REF}_{\mathrm{in}}=13 \mathrm{MHz} @ 1 \mathrm{Vp-p} ;$ <br> OUTPUT A = Inactive and No Connect; <br> $\mathrm{REF}_{\text {out }} \div 8 ; \phi \mathrm{V}, \phi \mathrm{R}, \mathrm{PD}_{\text {out }}, \mathrm{LD}=$ No Connect; $\mathrm{D}_{\text {in }}$, ENB, $\mathrm{CLK}=\mathrm{V}_{\mathrm{DD}}$ or GND, Phase Detector B Selected (Bit C6 = Low) | * | mA |

*The nominal value $=7 \mathrm{~mA}$. This is not a guaranteed limit.

ANALOG CHARACTERISTICS—CURRENT SOURCE/SINK OUTPUT—PDout
( $\mathrm{l}_{\text {out }} \leq 2 \mathrm{~mA}, \mathrm{~V}_{\mathrm{DD}}=\mathrm{V}_{\mathrm{CC}}=4.5$ to $5.5 \mathrm{~V}, \mathrm{~V}_{\mathrm{DD}} \leq \mathrm{V}_{\mathrm{PD}}$. Voltages Referenced to GND)

| Parameter | Test Condition | VPD | Guaranteed Limit | Unit |
| :---: | :---: | :---: | :---: | :---: |
| Maximum Source Current Variation (Part-to-Part) | MC145190: $\mathrm{V}_{\text {out }}=0.5 \times \mathrm{V}_{\text {PD }}$ | 8.0 | $\pm 20$ | \% |
|  |  | 9.5 | $\pm 20$ |  |
|  | MC145191: $\mathrm{V}_{\text {out }}=0.5 \times \mathrm{V}_{\text {PD }}$ | 4.5 | $\pm 20$ | \% |
|  |  | 5.5 | $\pm 20$ |  |
| Maximum Sink-vs-Source Mismatch (Note 3) | MC145190: $\mathrm{V}_{\text {Out }}=0.5 \times \mathrm{V}_{\text {PD }}$ | 8.0 | 12 | \% |
|  |  | 9.5 | 12 |  |
|  | MC145191: $\mathrm{V}_{\text {out }}=0.5 \times \mathrm{V}_{\text {PD }}$ | 4.5 | 12 | \% |
|  |  | 5.5 | 12 |  |
| Output Voltage Range (Note 3) | MC145190: I $_{\text {out }}$ Variation $\leq 20 \%$ | 8.0 | 0.5 to 7.5 | V |
|  |  | 9.5 | 0.5 to 9.0 |  |
|  | MC145191: Iout Variation $\leq 20 \%$ | 4.5 | 0.5 to 4.0 | V |
|  |  | 5.5 | 0.5 to 5.0 |  |

NOTES:

1. Percentages calculated using the following formula: (Maximum Value - Minimum Value)/Maximum Value.
2. See Rx Pin Description for external resistor values.
3. This parameter is guaranteed for a given temperature within $-40^{\circ}$ to $+85^{\circ} \mathrm{C}$.

AC INTERFACE CHARACTERISTICS (VDD $=4.5$ to $5.5 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=-40$ to $+85^{\circ} \mathrm{C}, \mathrm{C}_{\mathrm{L}}=50 \mathrm{pF}$, Input $\mathrm{t}_{\mathrm{r}}=\mathrm{t}_{\mathrm{f}}=10 \mathrm{~ns}$;
MC145190: $\mathrm{V}_{\mathrm{PD}}=8.0$ to 9.5 V ; MC145191: $\mathrm{V}_{\mathrm{PD}}=4.5$ to 5.5 V with $\left.\mathrm{V}_{\mathrm{DD}} \leq \mathrm{V}_{\mathrm{PD}}\right)$

| Symbol | Parameter | Figure No. | Guaranteed Limit | Unit |
| :---: | :---: | :---: | :---: | :---: |
| ${ }_{\mathrm{c}}^{\mathrm{clk}}$ | Serial Data Clock Frequency (Note: Refer to Clock $\mathrm{t}_{\mathrm{w}}$ below) | 1 | dc to 4.0 | MHz |
| tPLH, tPHL | Maximum Propagation Delay, CLK to OUTPUT A (Selected as Data Out) | 1,5 | 105 | ns |
| tPLH, tPHL | Maximum Propagation Delay, ENB to OUTPUT A (Selected as Port) | 2, 5 | 100 | ns |
| tPZL, tPLZ | Maximum Propagation Delay, ENB to OUTPUT B | 2, 6 | 120 | ns |
| ${ }^{\text {tTLH, }}$, tTHL | Maximum Output Transition Time, OUTPUT A and OUTPUT B; tTHLONLY, on OUTPUT B | 1, 5, 6 | 100 | ns |
| $\mathrm{C}_{\text {in }}$ | Maximum Input Capacitance - $\mathrm{Din}_{\text {in }}$, $\overline{\text { ENB }}$, CLK |  | 10 | pF |

## TIMING REQUIREMENTS

$\left(\mathrm{V}_{\mathrm{DD}}=\mathrm{V}_{\mathrm{CC}}=4.5\right.$ to $5.5 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=-40$ to $+85^{\circ} \mathrm{C}$, Input $\mathrm{t}_{\mathrm{r}}=\mathrm{t}_{\mathrm{f}}=10 \mathrm{~ns}$ unless otherwise indicated)

| Symbol | Parameter | Figure No. | Guaranteed Limit | Unit |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{t}_{\text {su }}$, $\mathrm{th}^{\text {r }}$ | Minimum Setup and Hold Times, Din vs CLK | 3 | 20 | ns |
| tsu, th, trec | Minimum Setup, Hold and Recovery Times, ENB vs CLK | 4 | 100 | ns |
| $\mathrm{t}_{\mathrm{w}}$ | Minimum Pulse Width, ENB | 4 | * | cycles |
| $t_{\text {w }}$ | Minimum Pulse Width, CLK | 1 | 125 | ns |
| $\mathrm{tr}_{\mathrm{r}} \mathrm{tf}$ | Maximum Input Rise and Fall Times - CLK | 1 | 100 | $\mu \mathrm{s}$ |

[^0]
## SWITCHING WAVEFORMS



Figure 1.


Figure 3.


Figure 5. Test Circuit


Figure 2.


Figure 4.

*Includes all probe and fixture capacitance.

Figure 6. Test Circuit

LOOP SPECIFICATIONS ( $\mathrm{V}_{\mathrm{DD}}=\mathrm{V}_{\mathrm{C}}=4.5$ to 5.5 V unless otherwise indicated, $\mathrm{T}_{\mathrm{A}}=-40$ to $+85^{\circ} \mathrm{C}$ )

| Symbol | Parameter |  | Test Condition | Figure No. | Guaranteed Operating Range |  | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min |  | Max |  |
| $\mathrm{V}_{\text {in }}$ | Input Voltage Range, fin |  |  | $\begin{aligned} & 100 \mathrm{MHz} \leq \mathrm{f}_{\text {in }}<250 \mathrm{MHz} \\ & 250 \mathrm{MHz} \leq \mathrm{f}_{\text {in }} \leq 1100 \mathrm{MHz} \end{aligned}$ | 7 | $\begin{aligned} & 400 \\ & 200 \end{aligned}$ | $\begin{aligned} & 1500 \\ & 1500 \end{aligned}$ | mV p-p |
| ${ }^{\text {fref }}$ | Input Frequency Range, REFin Externally Driven in Reference Mode | MC145190 <br> MC145191 | $\begin{aligned} & V_{\text {in }} \geq 400 \mathrm{mV} \mathrm{p}-\mathrm{p} \\ & \mathrm{~V}_{\text {in }} \geq 1 \mathrm{Vp-p} \\ & V_{\text {in }} \geq 400 \mathrm{mV} \mathrm{p}-\mathrm{p} \\ & \mathrm{~V}_{\text {in }} \geq 1 \mathrm{~V}-\mathrm{p} \end{aligned}$ | 8 | $\begin{gathered} \hline 13 \\ 6^{*} \\ 12 \\ 4.5^{\star} \end{gathered}$ | $\begin{aligned} & 27 \\ & 27 \\ & 27 \\ & 27 \end{aligned}$ | MHz |
| ${ }^{\text {f }}$ XTAL | Crystal Frequency, Crystal Mode |  | $\mathrm{C} 1 \leq 30 \mathrm{pF}, \mathrm{C} 2 \leq 30 \mathrm{pF}$, Includes Stray Capacitance | 9 | 2 | 15 | MHz |
| $\mathrm{f}_{\text {out }}$ | Output Frequency, REF ${ }_{\text {out }}$ |  | $\mathrm{C}_{\mathrm{L}}=30 \mathrm{pF}$ | 10, 12 | dc | 10 | MHz |
| $f$ | Operating Frequency of the Phase Detectors |  |  |  | dc | 2 | MHz |
| ${ }^{\text {w }}$ w | Output Pulse Width, ¢R, ¢V, LD | MC145190 MC145191 | $\mathrm{f}_{\mathrm{R}}$ in Phase with $\mathrm{fV}_{\mathrm{V}}, \mathrm{C}_{\mathrm{L}}=50 \mathrm{pF}$, $\mathrm{V}_{P D}=5.5 \mathrm{~V}, \mathrm{~V}_{\mathrm{DD}}=\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}$ | 11, 12 | 17 | 85 | ns |
| $\begin{aligned} & \text { tTLH, } \\ & \text { tTHL } \end{aligned}$ | Output Transition Times, LD, $\phi$ V, QR - MC145191 $^{\prime}$ |  | $\begin{aligned} & C_{L}=50 \mathrm{pF}, \mathrm{~V}_{\mathrm{PD}}=5.5 \mathrm{~V}, \\ & \mathrm{~V}_{\mathrm{DD}}=\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V} \end{aligned}$ | 11, 12 | - | 65 | ns |
| $\mathrm{C}_{\text {in }}$ | Input Capacitance, REF in |  |  |  | - | 5 | pF |

*If lower frequency is desired, use wave shaping or higher amplitude sinusoidal signal.


Figure 7. Test Circuit


Figure 9. Test Circuit - Crystal Mode


Figure 8. Test Circuit — Reference Mode


Figure 10. Switching Waveform


Figure 11. Switching Waveform


Figure 12. Test Circuit

NORMALIZED INPUT IMPEDANCE AT $\mathrm{f}_{\mathrm{in}}$ - SERIES FORMAT ( $\mathrm{R}+\mathrm{jX}$ )
( 100 MHz to 1.1 GHz )


| Marker | Frequency <br> $(\mathbf{M H z})$ | Resistance <br> $(\Omega)$ | Capacitive <br> Reactance $(\Omega)$ | Capacitance <br> $(\mathrm{pF})$ |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 100 | 338 | -785 | 2.03 |
| 2 | 500 | 20.2 | -183 | 1.74 |
| 3 | 800 | 11.5 | -109 | 1.83 |
| 4 | 1100 | 8.2 | -70.2 | 2.06 |

RETURN LOSS AT $\mathbf{f}_{\text {in }}$


STANDING WAVE RATIO AT $\mathbf{f}_{\mathrm{in}}$


| Marker | Frequency <br> $(\mathbf{M H z})$ | SWR | Return Loss <br> (dB) |
| :---: | :---: | :---: | :---: |
| 1 | 100 | 43.7 | 0.40 |
| 2 | 500 | 34.7 | 0.48 |
| 3 | 800 | 25.3 | 0.68 |
| 4 | 1100 | 17.9 | 0.98 |

## PIN DESCRIPTIONS

## DIGITAL INTERFACE PINS

## $D_{\text {in }}$ <br> Serial Data Input (Pin 19)

The bit stream begins with the most significant bit (MSB) and is shifted in on the low-to-high transition of CLK. The bit pattern is 1 byte ( 8 bits) long to access the $C$ or configuration register, 2 bytes ( 16 bits) to access the first buffer of the R register, or 3 bytes ( 24 bits) to access the A register (see Table 1). The values in the $C, R$, and $A$ registers do not change during shifting because the transfer of data to the registers is controlled by ENB.

## CAUTION

The value programmed for the N -counter must be greater than or equal to the value of the A -counter.
The 13 least significant bits (LSBs) of the R register are double-buffered. As indicated above, data is latched into the first buffer on a 16-bit transfer. (The 3 MSBs are not doublebuffered and have an immediate effect after a 16-bit transfer.) The second buffer of the $R$ register contains the 13 bits for the $R$ counter. This second buffer is loaded with the contents of the first buffer when the A register is loaded (a 24-bit transfer). This allows presenting new values to the R, A, and N counters simultaneously. If this is not required, then the 16-bit transfer may be followed by pulsing ENB low with no signal on the CLK pin. This is an alternate method of transferring data to the second buffer of the R register (see Figure 17).

The bit stream needs neither address nor steering bits due to the innovative BitGrabber registers. Therefore, all bits in the stream are available to be data for the three registers. Random access of any register is provided. That is, the registers may be accessed in any sequence. Data is retained in the registers over a supply range of 4.5 to 5.5 V . The formats are shown in Figures 15, 16, and 17.

Din typically switches near $50 \%$ of $V_{D D}$ to maximize noise immunity. This input can be directly interfaced to CMOS devices with outputs guaranteed to switch near rail-to-rail. When interfacing to NMOS or TTL devices, either a level shifter (MC74HC14A, MC14504B) or pull-up resistor of $1 \mathrm{k} \Omega$ to $10 \mathrm{k} \Omega$ must be used. Parameters to consider when sizing the resistor are worst-case lol of the driving device, maximum tolerable power consumption, and maximum data rate.

Table 1. Register Access
(MSBs are shifted in first; C0, R0, and A0 are the LSBs)

| Number <br> of Clocks | Accessed <br> Register | Bit <br> Nomenclature |
| :---: | :---: | :---: |
| 8 | C Register | $\mathrm{C} 7, \mathrm{C} 6, \mathrm{C} 5, \ldots, \mathrm{C} 0$ |
| 16 | R Register | R15, R14, R13, .., R0 |
| 24 | A Register | A23, A22, A21, .., A0 |
| Other Values $\leq 32$ <br> Values $>32$ | See Figure 13 <br> See Figures <br> $22-25$ |  |
|  |  |  |

## CLK <br> Serial Data Clock Input (Pin 18)

Low-to-high transitions on CLK shift bits available at the $D_{\text {in }}$ pin, while high-to-low transitions shift bits from OUTPUT A (when configured as Data Out, see Pin 16).

The 24-1/2-stage shift register is static, allowing clock rates down to dc in a continuous or intermittent mode.

Eight clock cycles are required to access the C register. Sixteen clock cycles are needed for the first buffer of the R register. Twenty-four cycles are used to access the A register. See Table 1 and Figures 15, 16, and 17. The number of clocks required for cascaded devices is shown in Figures 24 through 26.

CLK typically switches near $50 \%$ of $V_{D D}$ and has a Schmitt-triggered input buffer. Slow CLK rise and fall times are allowed. See the last paragraph of $\mathbf{D}_{\mathbf{i n}}$ for more information.

## NOTE

To guarantee proper operation of the power-on reset (POR) circuit, the CLK pin must be held at GND (with $\overline{E N B}$ being a don't care) or $\overline{\text { ENB }}$ must be held at the potential of the $V+$ pin (with CLK being a don't care) during power-up. As an alternative, the bit sequence of Figure 13 may be used.

## ENB

## Active Low Enable Input (Pin 17)

This pin is used to activate the serial interface to allow the transfer of data to/from the device. When ENB is in an inactive high state, shifting is inhibited and the port is held in the initialized state. To transfer data to the device, ENB (which must start inactive high) is taken low, a serial transfer is made via $D_{\text {in }}$ and CLK, and ENB is taken back high. The low-to-high transition on ENB transfers data to the C or A registers and first buffer of the $R$ register, depending on the data stream length per Table 1.

## NOTE

Transitions on ENB must not be attempted while CLK is high. This puts the device out of synchronization with the microcontroller. Resynchronization occurs whenever ENB is high and CLK is low.
This input is also Schmitt-triggered and switches near $50 \%$ of VDD, thereby minimizing the chance of loading erroneous data into the registers. See the last paragraph of $\mathrm{D}_{\mathrm{in}}$ for more information.

For POR information, see the note for the CLK pin.

## OUTPUT A <br> Configurable Digital Output (Pin 16)

OUTPUT A is selectable as fR , fV , Data Out, or Port. Bits A22 and A23 in the A register control the selection; see Figure 16.

If A23 = A22 = high, OUTPUT A is configured as $f_{R}$. This signal is the buffered output of the 13-stage $R$ counter. The $f_{R}$ signal appears as normally low and pulses high, and can be used to verify the divide ratio of the R counter. This ratio extends from 5 to 8191 and is determined by the binary value loaded into bits R0-R12 in the R register. Also, direct access to the phase detectors via the REFin pin is allowed by choosing a divide value of 1 (see Figure 17). The maximum frequency at which the phase detectors operate is 2 MHz . Therefore, the frequency of $f_{R}$ should not exceed 2 MHz .

If A23 = high and A22 = low, OUTPUT A is configured as $\mathrm{f} V$. This signal is the buffered output of the $12-$ stage N counter. The fV signal appears as normally low and pulses high, and can be used to verify the operation of the prescaler,

A counter, and $N$ counter. The divide ratio between the $f_{\text {in }}$ input and the fV signal is $\mathrm{N} \times 64+\mathrm{A}$. N is the divide ratio of the N counter and A is the divide ratio of the A counter. These ratios are determined by bits loaded into the A register. See Figure 16. The maximum frequency at which the phase detectors operate is 2 MHz . Therefore, the frequency of $\mathrm{f} V$ should not exceed 2 MHz .

If A23 = low and A22 = high, OUTPUT A is configured as Data Out. This signal is the serial output of the 24-1/2-stage shift register. The bit stream is shifted out on the high-to-low transition of the CLK input. Upon power up, OUTPUT A is automatically configured as Data Out to facilitate cascading devices.

If A23 = A22 = low, OUTPUT A is configured as Port. This signal is a general-purpose digital output which may be used as an MCU port expander. This signal is low when the Port bit (C1) of the C register is low, and high when the Port bit is high.

## OUTPUT B <br> Open-Drain Digital Output (Pin 15)

This signal is a general-purpose digital output which may be used as an MCU port expander. This signal is low when the Out $B$ bit ( CO ) of the $C$ register is low. When the Out $B$ bit is high, OUTPUT $B$ assumes the high-impedance state. OUTPUT B may be pulled up through an external resistor or active circuitry to any voltage less than or equal to the potential of the VPD pin. Note: the maximum voltage allowed on the VPD pin is 9.5 V for the MC145190 and 5.5 V for the MC145191.

Upon power-up, power-on reset circuitry forces OUTPUT $B$ to a low level.

## REFERENCE PINS

## REF $_{\text {in }}$ and REF $_{\text {out }}$

Reference Input and Reference Output (Pins 20 and 1)
Configurable pins for a Crystal or an External Reference. This pair of pins can be configured in one of two modes: the crystal mode or the reference mode. Bits R13, R14, and R15 in the R register control the modes as shown in Figure 17.

In crystal mode, these pins form a reference oscillator when connected to terminals of an external parallel-resonant crystal. Frequency-setting capacitors of appropriate values as recommended by the crystal supplier are connected from each of the two pins to ground (up to a maximum of 30 pF each, including stray capacitance). An external resistor of $1 \mathrm{M} \Omega$ to $15 \mathrm{M} \Omega$ is connected directly across the pins to ensure linear operation of the amplifier. The device is designed to operate with crystals up to 15 MHz ; the required connections are shown in Figure 9. To turn on the oscillator, bits R15, R14, and R13 must have an octal value of one (001 in binary, respectively). This is the active-crystal mode shown in Figure 17. In this mode, the crystal oscillator runs and the R Counter divides the crystal frequency, unless the part is in standby. If the part is placed in standby via the $C$ register, the oscillator runs, but the $R$ counter is stopped. However, if bits R15 to R13 have a value of 0, the oscillator is stopped, which saves additional power. This is the shutdown crystal mode (shown in Figure 17) and can be engaged whether in standby or not.

In the reference mode, REFin (Pin 20) accepts a signal up to 27 MHz from an external reference oscillator, such as a TCXO. A signal swinging from at least the $\mathrm{V}_{\mathrm{IL}}$ to $\mathrm{V}_{\mathrm{IH}}$ levels
listed in the Electrical Characteristics table may be directly coupled to the pin. If the signal is less than this level, ac coupling must be used as shown in Figure 8. Due to an onboard resistor which is engaged in the reference modes, an external biasing resistor tied between REFin and REF out is $^{\text {in }}$ not required.

With the reference mode, the REF out $^{\text {pin }}$ is configured as the output of a divider. As an example, if bits R15, R14, and R13 have an octal value of seven, the frequency at REF ${ }_{\text {out }}$ is the REFin frequency divided by 16. In addition, Figure 17 shows how to obtain ratios of eight, four, and two. A ratio of one-to-one can be obtained with an octal value of three. Upon power up, a ratio of eight is automatically initialized. The maximum frequency capability of the $R E F_{\text {out }}$ pin is 10 MHz . Therefore, for REFin frequencies above 10 MHz , the one-to-one ratio may not be used. Likewise, for REFin frequencies above 20 MHz , the ratio must be more than two.

If REF ${ }_{\text {out }}$ is unused, an octal value of two should be used for R15, R14, and R13 and the REF out pin should be floated. A value of two allows REFin to be functional while disabling REF $_{\text {out }}$, which minimizes dynamic power consumption and electromagnetic interference (EMI).

## LOOP PINS

$\mathrm{f}_{\mathrm{in}}$ and $\overline{\mathrm{f}_{\mathrm{in}}}$

## Frequency Inputs (Pins 11 and 10)

These pins are frequency inputs from the VCO. These pins feed the on-board RF amplifier which drives the 64/65 prescaler. These inputs may be fed differentially. However, they usually are used in a single-ended configuration (shown in Figure 7). Note that $f_{i n}$ is driven while $\overline{f_{i n}}$ must be tied to ground via a capacitor.

Motorola does not recommend driving $\overline{f_{i n}}$ while terminating $f_{i n}$ because this configuration is not tested for sensitivity. The sensitivity is dependent on the frequency as shown in the Loop Specifications table.

## PDout <br> Single-Ended Phase/Frequency Detector Output (Pin 6)

This is a three-state current-source/sink output for use as a loop error signal when combined with an external low-pass filter. The phase/frequency detector is characterized by a linear transfer function (no dead zone). The operation of the phase/frequency detector is described below and is shown in Figure 18.

POL bit (C7) in the C register = low (see Figure 15)
Frequency of $f V>f_{R}$ or Phase of $f V$ Leading $f_{R}$ : currentsinking pulses from a floating state
Frequency of $f V<f_{R}$ or Phase of $f V$ Lagging $f_{R}$ : currentsourcing pulses from a floating state
Frequency and Phase of $f V=f_{R}$ : essentially a floating state; voltage at pin determined by loop filter
POL bit (C7) = high
Frequency of $f V>f_{R}$ or Phase of $f V$ Leading $f_{R}$ : currentsourcing pulses from a floating state
Frequency of $\mathrm{f}_{\mathrm{V}}<\mathrm{f}_{\mathrm{R}}$ or Phase of $\mathrm{f}_{\mathrm{V}}$ Lagging $\mathrm{f}_{\mathrm{R}}$ : currentsinking pulses from a floating state
Frequency and Phase of $f_{V}=f_{R}$ : essentially a floating state; voltage at pin determined by loop filter
This output can be enabled, disabled, and inverted via the C register. If desired, $\mathrm{PD}_{\text {out }}$ can be forced to the floating state by utilization of the disable feature in the C register (bit C6). This is a patented feature. Similarly, $\mathrm{PD}_{\text {out }}$ is forced to the
floating state when the device is put into standby (STBY bit $\mathrm{C} 4=$ high $)$.

The PD ${ }_{\text {out }}$ circuit is powered by VPD. The phase detector gain is controllable by bits C3, C2, and C1: gain (in amps per radian) $=P D_{\text {out }}$ current divided by $2 \pi$.

## $\phi \mathbf{R}$ and $\phi \mathrm{V}$ (Pins 3 and 4)

## Double-Ended Phase/Frequency Detector Outputs

These outputs can be combined externally to generate a loop error signal. Through use of a Motorola patented technique, the detector's dead zone has been eliminated. Therefore, the phase/frequency detector is characterized by a linear transfer function. The operation of the phase/ frequency detector is described below and is shown in Figure 18.

POL bit (C7) in the C register = low (see Figure 15)
Frequency of $f V>f R$ or Phase of $f V$ Leading $f R: \phi V=$ negative pulses, $\phi \mathrm{R}=$ essentially high
Frequency of $f \mathrm{~V}<\mathrm{f}_{\mathrm{R}}$ or Phase of fV L Lagging $\mathrm{f}_{\mathrm{R}}: \phi \mathrm{V}=$ essentially high, $\phi \mathrm{R}=$ negative pulses
Frequency and Phase of $f V=f_{R}: \phi V$ and $\phi R$ remain essentially high, except for a small minimum time period when both pulse low in phase
POL bit (C7) = high
Frequency of $f V>f_{R}$ or Phase of $f V$ Leading $f R: \phi R=$ negative pulses, $\phi \mathrm{V}=$ essentially high
Frequency of $f V<f_{R}$ or Phase of $f V$ Lagging $f R: \phi R=$ essentially high, $\phi \mathrm{V}=$ negative pulses
Frequency and Phase of $f V=f_{R}: \phi V$ and $\phi R$ remain essentially high, except for a small minimum time period when both pulse low in phase
These outputs can be enabled, disabled, and interchanged via C register bits C 6 or C 4 . This is a patented feature. Note that when disabled or in standby, $\phi \mathrm{R}$ and $\phi \mathrm{V}$ are forced to their rest condition (high state).

The $\phi \mathrm{R}$ and $\phi \mathrm{V}$ output signal swing is approximately from GND to VPD.

## LD

## Lock Detector Output (Pin 2)

This output is essentially at a high level with narrow low-going pulses when the loop is locked ( $f R$ and $f v$ of the same phase and frequency). The output pulses low when $f_{V}$ and $f_{R}$ are out of phase or different frequencies. LD is the logical ANDing of $\phi R$ and $\phi V$ (see Figure 18).

This output can be enabled and disabled via the $C$ register. This is a patented feature. Upon power up, on-chip initialization circuitry disables LD to a static low logic level to prevent a false "lock" signal. If unused, LD should be disabled and left open.

The LD output signal swing is approximately from GND to VDD.
Rx

## External Resistor (Pin 8)

A resistor tied between this pin and GND, in conjunction with bits in the C register, determines the amount of current that the $\mathrm{PD}_{\text {out }}$ pin sinks and sources. When bits C2 and C3 are both set high, the maximum current is obtained at $\mathrm{PD}_{\text {out }}$; see Tables 2 and 3 for other values of current. To achieve a maximum current of 2 mA , the resistor should be about $47 \mathrm{k} \Omega$ when $\mathrm{V}_{P D}$ is 9 V or about $18 \mathrm{k} \Omega$ when $\mathrm{V}_{P D}$ is 5.0 V . See Figure 14 if lower maximum current values are desired.

When the $\phi \mathrm{R}$ and $\phi \mathrm{V}$ outputs are used, the Rx pin may be floated.

## TEST POINT PINS

## TEST 1

## Modulus Control Signal (Pin 9)

This pin may be used in conjunction with the Test 2 pin for access to the on-board $64 / 65$ prescaler. When Test 1 is low, the prescaler divides by 65. When high, the prescaler divides by 64 .

## CAUTION

This pin is an unbuffered output and must be floated in an actual application. This pin must be attached to an isolated pad with no trace.

## TEST 2

## Prescaler Output (Pin 13)

This pin may be used to access to the on-board 64/65 prescaler output.

## CAUTION

This pin is an unbuffered output and must be floated in an actual application. This pin must be attached to an isolated pad with no trace.

## POWER SUPPLY PINS

## VDD <br> Positive Power Supply (Pin 14)

This pin supplies power to the main CMOS digital portion of the device. The voltage range is +4.5 to +5.5 V with respect to the GND pin.

For optimum performance, VDD should be bypassed to GND using a low-inductance capacitor mounted very close to these pins. Lead lengths on the capacitor should be minimized.

## VCC <br> Positive Power Supply (Pin 12)

This pin supplies power to the RF amp and 64/65 prescaler. The voltage range is +4.5 to +5.5 V with respect to the GND pin. In the standby mode, the VCC pin still draws a few milliamps from the power supply. This current drain can be eliminated with the use of transistor Q1 as shown in Figure 22.

For optimum performance, VCC should be bypassed to GND using a low-inductance capacitor mounted very close to these pins. Lead lengths on the capacitor should be minimized.

## VPD <br> Positive Power Supply (Pin 5)

This pin supplies power to both phase/frequency detectors $A$ and $B$. The voltage applied on this pin must be no less than the potential applied to the VDD pin. The maximum voltage can be +9.5 V with respect to the GND pin for the MC145190 and +5.5 V for the MC145191.

For optimum performance, VPD should be bypassed to GND using a low-inductance capacitor mounted very close to these pins. Lead lengths on the capacitor should be minimized.

## GND <br> Ground (Pin 7)

Common ground.


NOTE: It may not be convenient to control the ENB or CLK pins during power up per the Pin Descriptions. If this is the case, the part may be initialized through the serial port as shown in the figure above. The sequence is similar to accessing the registers except that the CLK must remain high at least 100 ns after ENB is brought high. Note that 3 groups of 5 bits are needed.

Figure 13. Initializing the PLL through the Serial Port

MC145190
Nominal PDout Spurious Current vs $f_{R}$ Frequency
(1 V < PD out < VPD-1 V)

| $\mathbf{f R}_{\mathbf{R}}$ <br> $(\mathbf{k H z})$ | Current <br> $(\mathbf{R M S} \mathbf{~ n A ) ~}$ |
| :---: | :---: |
| 10 | 1.6 |
| 20 | 5.3 |
| 50 | 22 |
| 100 | 95 |
| 200 | 320 |

MC145191
Nominal PDout Spurious Current vs $f_{R}$ Frequency

| $\underset{(\mathrm{kHz})}{\mathrm{fR}_{\mathrm{R}}}$ | Current (RMS nA) |
| :---: | :---: |
| 10 | 3.6 |
| 20 | 4.6 |
| 50 | 17 |
| 100 | 75 |
| 200 | 244 |

NOTE: For information on spurious current measurement see AN1253/D, "An Improved PLL Design Method Without $\omega_{\mathrm{n}}$ and $\zeta$ ".

Table 2. PDout Current, C1 = Low with OUTPUT A NOT Selected as "Port"; Also, Default Mode When OUTPUT A Selected as "Port"

| C3 | C2 | PD $_{\text {out }}$ Current |
| :---: | :---: | :---: |
| 0 | 0 | $70 \%$ |
| 0 | 1 | $80 \%$ |
| 1 | 0 | $90 \%$ |
| 1 | 1 | $100 \%$ |

Table 3. PDout Current, C1 = High with OUTPUT A NOT Selected as "Port"

| C3 | C2 | PD $_{\text {out }}$ Current |
| :---: | :---: | :---: |
| 0 | 0 | $25 \%$ |
| 0 | 1 | $50 \%$ |
| 1 | 0 | $75 \%$ |
| 1 | 1 | $100 \%$ |




Nominal MC145191 PDout Source Current vs Rx Resistance
NOTE: The MC145191 is optimized for Rx values in the $18 \mathrm{k} \Omega$ to $40 \mathrm{k} \Omega$ range. For example, to achieve 0.3 mA of output current, it is preferable to use a $30-k \Omega$ resistor for $R x$ and bit settings for $25 \%$ (as shown in Table 3 ).

Figure 14.


* At this point, the new byte is transferred to the C register and stored. No other registers are affected.

$$
\begin{array}{ll}
\text { C7 - POL: } & \begin{array}{l}
\text { Selects the output polarity of the phase/frequency detectors. When set high, this bit inverts the polarity } \\
\text { of PD out and interchanges the } \phi R \text { function with } \phi \text { V as depicted in Figure } 18 \text {. Also see the phase detector } \\
\text { output pin descriptions for more information. This bit is cleared low at power up. }
\end{array} \\
\text { C6-PDA/B: } & \begin{array}{l}
\text { Selects which phase/frequency detector is to be used. When set high, enables the output of phase/ } \\
\text { frequency detector A (PDout) and disables phase/frequency detector B by forcing } \phi \mathrm{R} \text { and } \phi \mathrm{V} \text { to the } \\
\text { static high state. When cleared low, phase/frequency detector B is enabled ( } \phi R \text { and } \phi V \text { ) and phase/ } \\
\text { frequency detector A is disabled with PD }
\end{array} \text { out forced to the high-impedance state. This bit is cleared } \\
\text { low at power up. }
\end{array}
$$ forces OUTPUT B low. The Out B bit is not affected by the standby mode. This bit is cleared low at power up.

Figure 15. C Register Access and Format (8 Clock Cycles are Used)



NOTES:

1. A power-on initialize circuit forces the OUTPUT A function to default to Data Out.
2. The values programmed for the $N$ counter must be greater than or equal to the values programmed for the $A$ counter. This results in a total divide value $=N \times 64+A$.
3. At this point, the three new bytes are transferred to the A register. In addition, the 13 LSBs in the first buffer of the R register are transferred to the R register's second buffer. Thus, the R, N, and A counters can be presented new divide ratios at the same time. The first buffer of the R register is not affected. The C register is not affected.


Figure 17. R Register Access and Format (16 Clock Cycles Are Used)


Figure 18. Phase/Frequency Detectors and Lock Detector Output Waveforms

## DESIGN CONSIDERATIONS

## CRYSTAL OSCILLATOR CONSIDERATIONS

The following options may be considered to provide a reference frequency to Motorola's CMOS frequency synthesizers.

## Use of a Hybrid Crystal Oscillator

Commercially available temperature-compensated crystal oscillators (TCXOs) or crystal-controlled data clock oscillators provide very stable reference frequencies. An oscillator capable of CMOS logic levels at the output may be direct or dc coupled to REFin. If the oscillator does not have CMOS logic levels on the outputs, capacitive or ac coupling to REF in may be used (see Figure 8).

For additional information about TCXOs and data clock oscillators, please consult the latest version of the eem Electronic Engineers Master Catalog, the Gold Book, or similar publications.

## Design an Off-Chip Reference

The user may design an off-chip crystal oscillator using discrete transistors or ICs specifically developed for crystal oscillator applications, such as the MC12061 MECL device. The reference signal from the MECL device is ac coupled to REFin (see Figure 8). For large amplitude signals (standard CMOS logic levels), dc coupling may be used.

## Use of the On-Chip Oscillator Circuitry

The on-chip amplifier (a digital inverter) along with an appropriate crystal may be used to provide a reference source frequency. A fundamental mode crystal, parallel resonant at
the desired operating frequency, should be connected as shown in Figure 19.

The crystal should be specified for a loading capacitance $\left(C_{L}\right)$ which does not exceed approximately 20 pF when used at the highest operating frequency of 15 MHz . Assuming R1 $=0 \Omega$, the shunt load capacitance $\left(\mathrm{C}_{\mathrm{L}}\right)$ presented across the crystal can be estimated to be:

$$
\mathrm{C}_{\mathrm{L}}=\frac{\mathrm{C}_{\text {in }} \mathrm{C}_{\text {out }}}{\mathrm{C}_{\text {in }}+\mathrm{C}_{\text {out }}}+\mathrm{C}_{\mathrm{a}}+\mathrm{C}_{\text {stray }}+\frac{\mathrm{C} 1 \cdot \mathrm{C}_{2}}{\mathrm{C} 1+\mathrm{C} 2}
$$

where

$$
\begin{aligned}
\mathrm{C}_{\mathrm{in}} & =5 \mathrm{pF}(\text { see Figure 20) } \\
\mathrm{C}_{\mathrm{out}} & =6 \mathrm{pF}(\text { see Figure 20) } \\
\mathrm{C}_{\mathrm{a}} & =1 \mathrm{pF}(\text { see Figure 20) }
\end{aligned}
$$

C1 and C2 = external capacitors (see Figure 19)
$\mathrm{C}_{\text {stray }}=$ the total equivalent external circuit stray capacitance appearing across the crystal terminals
The oscillator can be "trimmed" on-frequency by making a portion or all of C1 variable. The crystal and associated components must be located as close as possible to the REFin and $R E F_{\text {out }}$ pins to minimize distortion, stray capacitance, stray inductance, and startup stabilization time. Circuit stray capacitance can also be handled by adding the appropriate stray value to the values for $\mathrm{C}_{\text {in }}$ and $\mathrm{C}_{\text {out }}$. For this approach, the term $\mathrm{C}_{\text {stray }}$ becomes 0 in the above expression for $\mathrm{C}_{\mathrm{L}}$.

Power is dissipated in the effective series resistance of the crystal, $R_{e}$, in Figure 21. The maximum drive level specified by the crystal manufacturer represents the maximum stress that the crystal can withstand without damage or excessive shift in operating frequency. R1 in Figure 19 limits the drive level. The use of R1 is not necessary in most cases.

To verify that the maximum dc supply voltage does not cause the crystal to be overdriven, monitor the output
frequency ( f R ) at OUTPUT A as a function of supply voltage. ( $R^{\prime} F_{\text {out }}$ is not used because loading impacts the oscillator.) The frequency should increase very slightly as the dc supply voltage is increased. An overdriven crystal decreases in frequency or becomes unstable with an increase in supply voltage. The operating supply voltage must be reduced or R1 must be increased in value if the overdriven condition exists. The user should note that the oscillator start-up time is proportional to the value of R1.

Through the process of supplying crystals for use with CMOS inverters, many crystal manufacturers have developed expertise in CMOS oscillator design with crystals. Discussions with such manufacturers can prove very helpful (see Table 4).

## RECOMMENDED READING

Technical Note TN-24, Statek Corp.
Technical Note TN-7, Statek Corp.
E. Hafner, "The Piezoelectric Crystal Unit-Definitions and Method of Measurement", Proc. IEEE, Vol. 57, No. 2, Feb. 1969.
D. Kemper, L. Rosine, "Quartz Crystals for Frequency Control", Electro-Technology, June 1969.
P. J. Ottowitz, "A Guide to Crystal Selection", Electronic Design, May 1966.
D. Babin, "Designing Crystal Oscillators", Machine Design, March 7, 1985.
D. Babin, "Guidelines for Crystal Oscillator Design", Machine Design, April 25, 1985.


Figure 19. Pierce Crystal Oscillator Circuit


Figure 20. Parasitic Capacitances of the Amplifier and $\mathrm{C}_{\text {stray }}$


NOTE: Values are supplied by crystal manufacturer (parallel resonant crystal).

Figure 21. Equivalent Crystal Networks

Table 4. Partial List of Crystal Manufacturers

| Motorola - Internet Address |
| :---: |
| http://motorola.com $\quad$ (Search for resonators) |
| United States Crystal Corp. |
| Crystek Crystal |
| Statek Corp. |
| Fox Electronics |

NOTE: Motorola cannot recommend one supplier over another and in no way suggests that this is a complete listing of crystal manufacturers.
(A)


$$
\begin{aligned}
& \omega_{n}=\sqrt{\frac{K_{\phi} K_{V C O}}{N C}} \\
& \zeta=\frac{R}{2} \sqrt{\frac{K_{\phi} K V C O C}{N}}=\frac{\omega_{n} R C}{2}
\end{aligned}
$$

$$
Z(s)=\frac{1+s R C}{s C}
$$

NOTE:
For (A), using $K_{\phi}$ in amps per radian with the filter's impedance transfer function, $Z(s)$, maintains units of volts per radian for the detector/ filter combination. Additional sideband filtering can be accomplished by adding a capacitor $C^{\prime}$ across $R$. The corner $\omega_{C}=1 / R C^{\prime}$ should be chosen such that $\omega_{n}$ is not significantly affected.
(B)

$\omega_{n}=\sqrt{\frac{K_{\phi} K_{V C O}}{N_{C R}}}$

$$
\zeta=\frac{\omega_{n} \mathrm{R}_{2} \mathrm{C}}{2}
$$

ASSUMING GAIN A IS VERY LARGE, THEN:
$F(s)=\frac{R_{2} s C+1}{R_{1} s C}$
NOTE:
For (B), $R_{1}$ is frequently split into two series resistors; each resistor is equal to $R_{1}$ divided by 2. A capacitor $C_{C}$ is then placed from the midpoint to ground to further filter the error pulses. The value of $\mathrm{C}_{\mathrm{C}}$ should be such that the corner frequency of this network does not significantly affect $\omega_{n}$.

* The $\phi R$ and $\phi \vee$ outputs are fed to an external combiner/loop filter. The $\phi R$ and $\phi \vee$ outputs swing rail-to-rail. Therefore, the user should be careful not to exceed the common mode input range of the op amp used in the combiner/loop filter.
DEFINITIONS:
$\mathrm{N}=$ Total Division Ratio in Feedback Loop
$\mathrm{K}_{\phi}$ (Phase Detector Gain) $=\mathrm{I}_{\mathrm{PD}}$ Dout $/ 2 \pi$ amps per radian for $\mathrm{PD}_{\text {out }}$
$\mathrm{K}_{\phi}$ (Phase Detector Gain) $=\mathrm{V}_{\mathrm{PD}} / 2 \pi$ volts per radian for $\phi \mathrm{V}$ and $\phi \mathrm{R}$
$\mathrm{K}_{\mathrm{VCO}}\left(\mathrm{VCO}\right.$ Transfer Function) $=\frac{2 \pi \Delta \mathrm{f} \mathrm{VCO}}{\Delta \mathrm{V} \mathrm{VCO}}$ radians per volt
For a nominal design starting point, the user might consider a damping factor $\zeta_{\sigma} \approx 0.7$ and a natural loop frequency $\omega_{n} \approx\left(2 \pi f_{R} / 50\right)$ where $f_{R}$ is the frequency at the phase detector input. Larger $\omega_{n}$ values result in faster loop lock times and, for similar sideband filtering, higher $f_{R}-r e l a t e d$ VCO sidebands.

Either loop filter $(A)$ or $(B)$ is frequently followed by additional sideband filtering to further attenuate $\mathrm{f}_{\mathrm{R}}-$ related VCO sidebands. This additional filtering may be active or passive.

## RECOMMENDED READING:

Gardner, Floyd M., Phaselock Techniques (second edition). New York, Wiley-Interscience, 1979.
Manassewitsch, Vadim, Frequency Synthesizers: Theory and Design (second edition). New York, Wiley-Interscience, 1980.
Blanchard, Alain, Phase-Locked Loops: Application to Coherent Receiver Design. New York, Wiley-Interscience, 1976.
Egan, William F., Frequency Synthesis by Phase Lock. New York, Wiley-Interscience, 1981.
Rohde, Ulrich L., Digital PLL Frequency Synthesizers Theory and Design. Englewood Cliffs, NJ, Prentice-Hall, 1983.
Berlin, Howard M., Design of Phase-Locked Loop Circuits, with Experiments. Indianapolis, Howard W. Sams and Co., 1978.
Kinley, Harold, The PLL Synthesizer Cookbook. Blue Ridge Summit, PA, Tab Books, 1980.
Seidman, Arthur H., Integrated Circuits Applications Handbook, Chapter 17, pp. 538-586. New York, John Wiley \& Sons.
Fadrhons, Jan, "Design and Analyze PLLs on a Programmable Calculator," EDN. March 5, 1980.
AN535, Phase-Locked Loop Design Fundamentals, Motorola Semiconductor Products, Inc., 1970.
AR254, Phase-Locked Loop Design Articles, Motorola Semiconductor Products, Inc., Reprinted with permission from Electronic Design, 1987.
AN1253/D, An Improved PLL Design Method Without $\omega_{\mathrm{n}}$ and $\zeta$, Motorola Semiconductor Products, Inc., 1995.


NOTES:

1. When used, the $\phi \mathrm{R}$ and $\phi \mathrm{V}$ outputs are fed to an external combiner/loop filter. See the Phase-Locked Loop - Low-Pass Filter Design page for additional information.
2. Transistor Q1 is required only if the standby feature is needed. Q1 permits the bipolar section of the device to be shut down via use of the general-purpose digital pin, OUTPUT B. If the standby feature is not needed, tie Pin 12 directly to the power supply.
3. For optimum performance, bypass the $\mathrm{V}_{\mathrm{CC}}, \mathrm{V}_{\mathrm{DD}}$, and $\mathrm{V}_{P D}$ pins to $G N D$ with low-inductance capacitors.
4. The $R$ counter is programmed for a divide value $=R E F_{i n} / f_{R}$. Typically, $f_{R}$ is the tuning resolution required for the VCO. Also, the VCO frequency divided by $\mathrm{f}_{\mathrm{R}}=\mathrm{NT}=\mathrm{N} \times 64+\mathrm{A}$; this determines the values $(\mathrm{N}, \mathrm{A})$ that must be programmed into the N and A counters, respectively.

Figure 22. Example Application


NOTE: See related Figures 24 through 26; these bit streams apply to the MC145190, MC145191, MC145200, and MC145201.

Figure 23. Cascading Two Devices

## ARCHIVE INFORMATION


*At this point, the new bytes are transferred to the C registers of both devices and stored. No other registers are affected.


NOTES APPLICABLE TO EACH DEVICE:

1. At this point, bits R13, R14, and R15 are stored and sent to the "OSC or 4-Stage Divider" block in the Block Diagram. Bits R0 through R12 are loaded into the first buffer in the doublebuffered section of the $R$ register. Therefore, the $R$ counter divide ratio is not altered yet and retains the previous ratio loaded. The $C$ and $A$ registers are not affected.
2. At this point, the bits R0 through R12 are transferred to the second buffer of the $R$ register. The $R$ counter begins dividing by the new ratio after completing the rest of the present count cycle. CLK must be low during the ENB pulse, as shown. Also, see note of Figure 25 for an alternate method of loading the second buffer in the R register. The C and A registers are not affected. The first buffer of the R register is not affected.

## PACKAGE DIMENSIONS

F SUFFIX
SOG (SMALL OUTLINE GULL-WING) PACKAGE
CASE 751J-02

NOTES:
. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
CONTROLLING DIMENSION: MILLIMETER
DIMENSIONS A AND B DO NOT INCLUDE MOLD PROTRUSION.
MAXIMUM MOLD PROTRUSION 0.15 (0.006) PER SIDE.
5. DIMENSION D DOES NOT INCLUDE DAMBAR PROTRUSION. ALLOWABLE DAMBAR PROTRUSION SHALL BE 0.13 ( 0.005 ) TOTAL IN EXCESS OF THE D DIMENSION AT MAXIMUM MATERIAL CONDITION

| DIM | MILLIMETERS |  | INCHES |  |
| :---: | :---: | :---: | :---: | :---: |
|  | MIN | MAX | MIN | MAX |
| A | 12.55 | 12.80 | 0.494 | 0.504 |
| B | 5.10 | 5.40 | 0.201 | 0.213 |
| C | - | 2.00 | - | 0.079 |
| D | 0.35 | 0.45 | 0.014 | 0.018 |
| G | 1.27 | BSC | 0.050 BSC |  |
| J | 0.18 | 0.23 | 0.007 | 0.009 |
| K | 0.55 | 0.85 | 0.022 | 0.033 |
| L | 0.05 | 0.20 | 0.002 | 0.008 |
| M | $0^{\circ}$ | $7^{\circ}$ | $0^{\circ}$ | $7^{\circ}$ |
| S | 7.40 | 8.20 | 0.291 | 0.323 |

DT SUFFIX
TSSOP (THIN SHRUNK SMALL OUTLINE PACKAGE)
CASE 948D-03

NOTES:

1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
2. CONTROLLING DIMENSION: MILLIMETER.
3. DIMENSION A DOES NOT INCLUDE MOLD FLASH, PROTRUSIONS OR GATE BURRS. MOLD FLASH OR GATE BURRS SHALL NOT EXCEED 0.15 (0.006) PER SIDE.
4. DIMENSION B DOES NOT INCLUDE INTERLEAD FLASH OR PROTRUSION INTERLEAD FLASH OR PROTRUSION SHALL NOT EXCEED 0.25 (0.010) PER SIDE.
5. DIMENSION K DOES NOT INCLUDE DAMBAR PROTRUSION. ALLOWABLE DAMBAR PROTRUSION SHALL BE 0.08 (0.003) TOTAL IN PROTRUSION SHALL BE 0.08 (0.003) TOTALIN
EXCESS OF THE K DIMENSION AT MAXIMUM MATERIAL CONDITION
6. TERMINAL NUMBERS ARE SHOWN FOR REFERENCE ONLY.

DIMENSIONS A AND B ARE TO BE DETERMINED AT DATUM PLANE-U-.

|  | MILLIMETERS |  | INCHES |  |
| :---: | :---: | :---: | :---: | :---: |
| DIM | MIN | MAX | MIN | MAX |
| A | - | 6.60 | - | 0.260 |
| B | 4.30 | 4.50 | 0.169 | 0.177 |
| C | - | 1.20 | - | 0.047 |
| D | 0.05 | 0.25 | 0.002 | 0.010 |
| F | 0.45 | 0.55 | 0.018 | 0.022 |
| G | 0.65 BSC | 0.026 BSC |  |  |
| H | 0.275 | 0.375 | 0.011 | 0.015 |
| J | 0.09 | 0.24 | 0.004 | 0.009 |
| J1 | 0.09 | 0.18 | 0.004 | 0.007 |
| K | 0.16 | 0.32 | 0.006 | 0.013 |
| K1 | 0.16 | 0.26 | 0.006 | 0.010 |
| L | 6.30 | 6.50 | 0.248 | 0.256 |
| M | $0^{\circ}$ | $10^{\circ}$ | $0^{\circ}$ | $10^{\circ}$ |

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[^0]:    * The minimum limit is 3 REF in cycles or $195 \mathrm{f}_{\text {in }}$ cycles, whichever is greater.

